

The University of Sistan & Baluchestan Graduate School

The Dissertation of Ph.D. in Mechanical engineering

Title:

Inverse analysis of radiation heat transfer in participating medium with variable refractive index

Supervisors:

Dr. SM. Hosseini Sarvari Dr. A. Behzadmehr

Advisor:

Dr. SH. Mansouri

Research by:

Amin Namjoo

Feb. 2010

To my wife and my parents

Acknowledgments

I would like to express my deep gratitude to my thesis supervisor, Professor Hosseini Sarvari for his persistent support, inspiration and outstanding guidance. He has given me constant encouragements during this project. I am also deeply indebted to Professor Mansouri for devoting his valuable time to improve this research. I would like to thank Professor Behzadmehr for his support and wish to express my sincere gratitude and thanks to Professor Lemonnier for offer in me a six month sabbatical training in France. His valuable guidance together with Professor Le Dez are appreciated.

For my friend Dr. Seidi, Dr. Sarhadi, Dr. Abedini and Dr. Razaghi I offer my most sincere words of gratitude.

Finally, very special thanks go to my wife, my Parents, my brother and my sisters for their supports.

Amin Namjoo

Abstract

In many engineering and practical problems, the medium has a variable refractive index such as heating of glass, thermal protecting coating, manufacturing of waveguide materials, optical measurement of flam, thermal barrier coating, elctrochoromic windows, etc. The variation of refractive index may be a reason of the structure or thermal effect caused by spatial and temporal variations. Therefore, retrieving of temperature and refractive index distributions, that play important role in radiative transfer in graded index medium, is very practical. In the present work an inverse analysis of 1-D absorbing, emitting and scattering graded index medium is performed to determine the temperature and refractive index distribution. In the first part, a serious attention is devoted to the direct problem, since solving the direct problem is a basic step in all inverse algorithms. The conservative and non-conservative form of radiative transfer equation of graded index medium in general orthogonal curvilinear coordinate system are presented, which has not been done till now. This formulation is simplified for 1-D case and the constant quadrature discrete ordinate method is used to solve it. The advantageous of presented method is its ability to model arbitrary variation of refractive index, while the previous similar method can only model the monotonic variation of refractive index. In the second part, three different inverse problems are solved. First, the source term (temperature distribution) is estimated through the knowledge of exit intensities at boundary surface by the conjugate gradient method. Estimation of refractive index distribution in a graded index medium by inverse methods through measured radiative heat transfer parameters is completely a novel idea and has not been done yet. Hence, in the second problem, the simultaneous estimation of source term and linear refractive index distribution is done through the knowledge of exit intensities at boundary surfaces by the conjugate gradient method and a two dimensional searching network approach. In the last case the arbitrary distribution of refractive index distribution is retrieved by a combination of the conjugate gradient method and Levenberg-Marquardt method. The measured data is radiative intensities at boundary surfaces and radiative heat fluxes inside the medium.

Keywords: Graded index medium, inverse analysis, curvilinear coordinate system

List of Figurers

Figure 2-1 General orthogonal coordinate system and corresponding azimuthal and polar angles 2	21
Figure 2-2 Details of Cartesian coordinate system 3	39
Figure 2-3 Details of cylindrical coordinate system 4	40
Figure 3-1 Geometry of one-dimensional absorbing, emitting and scattering parallel-plane graded	1
index medium 4	46
Figure 3-2 division of (a) spatial domain (b) angular domain 4	47
Figure 3-3 Flowchart of calculating parameters that are needed in direction 5	50
Figure 3-4 Main flowchart of direct problem 5	51
Figure 4-1 The measured exit intensities at boundary surfaces 5	55
Figure 4-2 schematic of the searching network of finding refractive indices at boundary surfaces 6	60
Figure 5-1 Temperature field in a linear variation of refractive index $n = 1.2 + 0.6\tau / \tau_L$ with	
optical thickness of (a) $\tau_L = 0.01$ (b) $\tau_L = 3$ and emissivity of boundaries (1):	
$\varepsilon_0 = \varepsilon_L = 1.0$, (2): $\varepsilon_0 = \varepsilon_L = 0.7$, (3): $\varepsilon_0 = \varepsilon_L = 0.2$, (4): $\varepsilon_0 = 0.2, \varepsilon_L = 1.0$, (5):	
$\varepsilon_0 = 1.0, \varepsilon_L = 0.2$	71
Figure 5-2 Temperature field for a linear variation of refractive index and	
$\tau_L = 1.0, \omega = 0.2, n_0 = 1.0, (1): b = 0.0, (2): b = 1.0, (3): b = 3.0, (4): b = 5.0.7$	71
Figure 5-3 . The effect of error in measured data on estimation of source term, $S_1(\tau)$. (a) Root	
mean square error relative to the average source term (b) Maximum relative error. 7	75
Figure 5-4 Estimation of source term $S_1(\tau)$ for the most deviated case among 20 sample run of	
error in measured data (a) exact and estimated source distribution (b) relative error	
distribution of estimating source term 7	76
Figure 5-5 The convergence history for $\eta = 2\%$ and $\eta = 5\%$	76
Figure 5-6 The effect of error in measured data on estimation of source term, $S_2(\tau)$. (a) root	
mean square error relative to the average source term (b) maximum relative error. 7	77
Figure 5-7 Estimation of source term $S_2(\tau)$ for the 17 th sample run which shows more deviation	n
from exact source distribution at $\eta = 5\%$ (a) exact and estimated source distribution (b)	
relative error distribution. 7	78
Figure 5-8 The effect of error in measured data on estimation of source term, $S_3(au)$. (a) root	
mean square error relative to the average source term (b) maximum relative error 7	79
Figure 5-9 Estimation of source term $S_1(\tau)$ for 14 th sample run (a) exact and estimated source	
distribution (b) relative error distribution.	79

Figure 5-10 The effect of refractive index gradient on estimation of source term, $S_1(au)$. (a)	root
mean square error relative to the average source term (b) maximum relative error.	81
Figure 5-11 The effect of single scattering albedo on estimation of source term, $S_1(\tau)$. (a) is	oot
mean square error relative to the average source term (b) maximum relative error.	82
Figure 5-12 The effect of boundary emissivities on estimation of source term, $S_1(\tau)$. (a) ro	ot
mean square error relative to the average source term (b) maximum relative error.	82
Figure 5-13 The effect of optical thickness on estimation of source term, $S_4(au)$. (a) root me	an
square error relative to the average source term (b) maximum relative error.	83
Figure 5-14 The effect of error in system parameters and measured data on estimation of sour	ce
term, $S_1(au)$. (a) root mean square error relative to the average source term (b) maxim	um
relative error.	85
Figure 5-15 The effect of error in system parameters except refractive index at boundaries an	t
measured data on estimation of source term, $S_1(au)$. (a) root mean square error relativ	e to
the average source term (b) maximum relative error	86
Figure 5-16 Estimation of source term $S_1(\tau)$ for the most deviated E_{relm} among 20 sample	run
of error in all system parameters except refractive index at boundary surfaces and measured	ured
data (a) exact and estimated source distribution (b) relative error distribution.	86
Figure 5-17 Exact and estimated source term distribution (a) $S_1(\tau)$ (b) $S_2(\tau)$ (c) $S_3(\tau)$.	90
Figure 5-18 Estimation of source term $S_4(au)$ in the case of 1% error in measured data and t	wo
search step size $\Delta n = 0.1$ and $\Delta n = 0.05$ (a) exact and estimated source distribution	(b)
relative error distribution of the estimated source term	90
Figure 5-19 Estimated regions of source distribution for $S_1(\tau)$ for 20 different sample run for	or two
different normally distributed random errors (a) $\eta = 2\%$ (b) $\eta = 4\%$	92
Figure 5-20 Effect of normally distributed random errors on refractive indices at boundary su	rfaces
(a) $\eta = 2\%$ (b) $\eta = 4\%$	93
Figure 5-21 Effect of error in system parameters and measured data (a) 2% error in measured	data
(b) 2% error in both measured data and all system parameters (c) 2% error in measured	data
and system parameters except boundaries temperature.	93
Figure 5-22 The effect of system parameters on estimation of source term $S_1(au)$. (a) single	
scattering albedo (b) asymmetry scattering parameter (c) boundary emissivities (d) opti	cal
thickness.	95
Figure 5-23 The effect of optical thickness on estimation of refractive indeices at (a) lower	
boundary surfaces (b) upper boundary surfaces.	96

f

Figure 5-24 Comparing the refractive index estimation obtained from first and second approaches with 1% error in measured data for (a) $n_1(\tau)$, (b) $n_2(\tau)$, (c) $n_3(\tau)$. 102

Figure 5-25 The refractive index estimation from third approach (a) $n_1(\tau)$,(b) $n_2(\tau)$, (c) $n_3(\tau)$.

List of Tables

Table 5-1 Normalized heat flux across the slab at radiative equilibrium at different optical	
thickness and different variation of refractive index. (walls are black)	72
Table 5-2 radiative constant parameters used in the inverse estimation	74
Table 5-3 The maximum corresponding values of $E_{\rm rms}/S_{\rm ave}$ and $E_{\rm relm}$ for $S_1(\tau)$, $S_2(\tau)$ and	
$S_3(\tau)$ of 20 sample run	78
Table 5-4 Maximum values of E_{rms}/S_{ave} and E_{relm} for variation of radiative system parameters	S
in the medium	83
Table 5-5 Radiative constant parameters used in the inverse estimation	87
Table 5-6 The effect of different value of degree of polynomial on source and refractive index	
profile estimation	88
Table 5-7 The values of refractive indices at boundaries and E_{rms}/S_{ave} for different values of	
network search step size	90
Table 5-8 The maximum relative errors for estimation of refractive indices at boundary surfaces,	
and the maximum values of $E_{\rm rms}$ / $S_{\rm avg}$ and $E_{\rm relm}$ for 20 sample runs with different values	3
of errors in measured data	91
Table 5-9 Radiative constant parameters used in the inverse estimation	97
Table 5-10 Objective functions, maximum relative errors and estimated refractive indices at	
boundary surfaces for three different refractive index distributions obtained by first approach	1 98
Table 5-11 Objective function and maximum relative error for three type of refractive index	
distribution with different order of polynomial in the case of errorless measured data	
obtained by second approach	100
Table 5-12 Objective function and maximum relative error for three type of refractive index	
distribution with different order of polynomial in the case of 1% error in measured data	
obtained by second approach	100
Table 5-13 Objective function and maximum relative error for three kind of refractive index	
distribution in the case of 1% error in measured data obtained from third approach	101

Nomenclatures

a	Vector of unknown coefficients
С	Light velocity
d	Direction of descent
Ε	Error
g	Asymmetric scattering parameter
G	Minimum of objective function at each discrete point of network
h	Metric coefficient of coordinate system
Н	Global rotation of local coordinate system
F	objective function
Ι	radiation intensity
I_b	Blach body radiative intensity
J	Sensitivity matrix
L	Optical path
М	Number of angular elements
M'	Number of discrete point of each search parameter
Ν	Number of spatial elements
n	Refractive index
Р	Order of source polynomial
q	Radiative heat flux
r	Position vector
$S(\tau)$	Source term
S	Curvilinear abscissa along a path
S	Tangential unit vector to the path

Т	Temperature
W	Angular weight
Y	exit intensities on the surface boundaries
β	search step size
ε	Emissivity
ζ	random number
η	Error in measurements
η^*	Error in system parameters
ρ	Conjugation coefficient
ρ	Charectrizes the rotation of local coordinate system
ξ	Small positive number
К	Extinction coefficient
K _a	Absorption coefficient
K _s	Scattering coefficient
μ	Direction cosine
$\sigma_{_m}$	Standard deviation of measurement errors
σ	Stephan-Boltzman constant
τ	Optical thickness
Φ	Scattering phase function
ω	Single scattering albedo
Θ	Represent a system parameter
Subscript	
i	Center values of spatial slice

j

$i\pm 1/2$	Edge values of spatial slice with <i>i</i> center
k	Iteration number
m	Center value of angular segment
0	Boundary at $\tau = 0$
L	Boundary at $\tau = \tau_L$
rel	Relative
rms	Root mean square

Table of Contents

Chapter	r 1.	Introduction 1
1.1.	Intr	oduction 2
1.2.	Dif	ficulties in Solving Inverse Heat Transfer Problem
1.3.	Clas	ssification of Inverse Problems
1.4.	Inve	erse Radiative Heat Transfer and Graded Index Medium4
1.4	.1.	Direct Problem of Radiative Transfer in Graded Index Medium 6
1.4	.2.	Inverse Problem in Participating Medium
Chapte	r 2.	Conservative and non-Conservative Forms of Radiative Transfer
Equation	n of (Graded Index Medium in General Orthogonal Curvilinear Coordinate
System		17
2.1.	Rad	liative Transfer Equation in Graded Index Media18
2.2.	Mat	thematical Modeling
2.2	.1.	Optical Path
2.2	.2.	An expression for Fermat Principle 19
2.2	.3.	Orientation Change of Local Coordinate System
2.2	.4.	Variation of polar angles representing the direction of propagation26
2.3.	Rad	liation Transfer Equation
2.3	.1.	The general Form of Radiative transfer Equation
2.3	.2.	The Non-conservative Form of Transfer Operator
2.3	.3.	The conservative Form of Transfer Operator
2.4.	Spe	cial Cases
2.4	.1.	Cartesian Coordinate System
2.4	.2.	Cylindrical Coordinate System
2.4	.3.	Spherical Coordinate System
Chapter	r 3.	Numerical Method for Direct Problem

3.1. Intr	oduction	44
3.2. The	e Governing Equation	44
3.3. Bou	indary Conditions	45
3.4. Nur	merical Model	46
3.5. Inte	gration over a Control Volume	47
Chapter 4.	Inverse Method	52
4.1. Inve	erse Radiation Problem of Temperature Distribution i	in One-
Dimensior	nal Isotropically Scattering Participating Slab with	Variable
Refractive	Index	53
4.1.1.	The Direct Problem	54
4.1.2.	The Inverse Problem	54
4.1.3.	Sensitivity Problem	56
4.1.4.	Stopping Criterion	57
4.1.5.	Computational Algorithm	57
4.2. Sim	nultaneous estimation of source and refractive index distrib	oution in
one-dimen	sional absorbing-emitting and scattering graded index medium	m 58
4.2.1.	Direct Problem	58
4.2.2.	Inverse Problem	59
4.2.3.	Sensitivity Problem	62
4.2.4.	Stopping Criterion	63
4.2.5.	Computational algorithm for the searching of a	63
4.3. Esti	imation of arbitrary refractive index distribution in a one-dim	ensional
semitransp	parent graded index medium	
4.3.1.	First approach	64
4.3.2.	Second approach	65
4.3.3.	Third approach	68
Chapter 5.	Results and Discussions	69

5.1. Validation of the direct solution
5.2. Inverse Results
5.2.1. Inverse Radiation Problem of Temperature Distribution in One- Dimensional Isotropically Scattering Participating Slab with Variable
Refractive Index
5.2.2. Simultaneous estimation of source and refractive index distribution
in one-dimensional absorbing-emitting and scattering graded index medium
5.2.3. Estimation of arbitrary refractive index distribution in a one- dimensional semitransparent graded index medium
Chapter 6. Conclusion
Refrences

Chapter 1. Introduction

1.1. Introduction

Inverse problems are the problems that consist of finding an unknown property of an object, or a medium, from the observation of a response of this object, or medium, to a probing signal [1]. In the other words, in the direct problem the caused are given, the effect is determined; whereas in the inverse problem the effect is given, the cause (or causes) is determined. Thus, the theory of inverse problems yields a theoretical basis for remote sensing and non-destructive evaluation [1]. On mathematical physics view point, the aim of solving a direct problem is to find the solution of the partial differential equation with proper boundary and/or initial conditions. However, in an inverse problem governing differential equation is not completely defined or some of the boundary conditions or initial conditions are not specified, but some additional information is available. Through this information, the unknown conditions and parameters should be determined. [2]. Inverse analysis have a lot of practical and theoretical usage in all branches of science and engineering such as, physics, geophysics, hydrology, mathematics, astronomy, heat transfer and other disciplines. Inverse heat transfer problems are very important and practical. For example measurement of temperature in a furnace is a challenging problem. Due to the high temperature, the traditional thermometer is useless and we have to use more advanced methods. One possibility is to use ultrasound. The high temperature renders the gases in the furnace turbulent, thus changing their acoustic properties which in turn are reflected in the acoustic echoes. Now the forward model consists of the challenging problem of describing the turbulence as a function of temperature plus acoustic wave propagation in the medium, and its even more challenging inverse counterpart of determining the temperature from acoustic observations [3]. Also, aerodynamic heating of space vehicles is so high during reentry in the atmosphere that the surface temperature of the thermal shield cannot be measured directly with temperature sensors. Therefore, temperature sensors are placed beneath the hot surface of the shield and the surface temperature is recovered by inverse analysis [4].

1.2. Difficulties in Solving Inverse Heat Transfer Problem

Inverse heat transfer problems are classified as ill-posed problems in a mathematical sense, because their solution may become unstable as the measurements contain error. The solution of a problem should be satisfied the following three conditions to classify as a well-posed problem [4].

- 1. The solution must exist
- 2. The solution must be unique
- 3. The solution must be stable under small changes to the input

Compared to the well posed problem, the inverse problem may have no solution, or have multiple solutions. The main difficulty is that the solution may not be stable if there is error in input data. So we need special methods and algorithms to stabilize the solution. But, these methods do not guarantee the correct solution. Even if we get a stable solution for the inverse problem, it may not be acceptable as it is not the solution or the problem yields multiple solutions. So care must be taken during solving an inverse problem and the answers should always be looked as suspicious.

1.3. Classification of Inverse Problems

There are several classifications of inverse heat transfer problems related to the methods, usage, etc. Some of these classes are brought briefly in following lines: Inverse problem can be solved as parameters estimation or as function estimation approach. In parameters estimation approach a finite number of parameters are to be determined. These parameters can be constant thermophysical properties such as thermal conductivity or absorption coefficient of medium. Also if some information is available on the functional form of the unknown quantity, the inverse problem is reduced to the estimation of few unknown parameters. If such information is not available, inverse problem become function estimation in an infinite dimensional space of functions.

Inverse heat transfer can be also classified in accordance with the mode of heat transfer process, such as [4]

- 1. Inverse heat transfer of conduction
- 2. inverse heat transfer of convection
- 3. inverse heat transfer of surface radiation
- 4. inverse heat transfer in participating medium
- 5. inverse heat transfer of simultaneous conduction and radiation
- 6. inverse heat transfer of simultaneous conduction and convection
- 7. inverse heat transfer of phase change

Another classification can be one based on the type of causal characteristic to be estimated. For example:

- 1. Inverse heat transfer of boundary condition
- 2. Inverse heat transfer of thermophysical properties
- 3. Inverse heat transfer of initial condition
- 4. Inverse heat transfer of source term
- 5. Inverse heat transfer of geometric characteristics of a heated body

Inverse heat transfer problems can be one, two or three dimensional. Also they may be linear or nonlinear.

1.4. Inverse Radiative Heat Transfer and Graded Index Medium

Radiative heat transfer is important when the temperature of medium and/or boundaries is high. In these cases this mode of heat transfer is almost dominant to other modes of heat transfer. Also radiative heat transfer is the only mode of heat transfer that does not need material medium and can transfer across the vacuum (as the sun heats the earth). The medium is called participating if it affects the intensity rays that travel through it. The effects can be classified into two groups. One attenuates the intensities pass the medium, and the other has augmentation effects. Attenuation is due to absorption and out-scattering and augmentation is a result of emission and in-scattering. It is obvious that the radaitive heat transfer in a medium depends on the properties of the medium, such as absorption coefficient, scattering coefficient, refractive index and so on. One of the most important properties is the refractive index which is the ratio of the velocity of light in the vacuum to its value in the medium. In a medium with constant refractive index the intensity rays travel along a straight path, while in a medium with variable refractive index the rays travel along a curve path. In this case, if the medium experiences a continuous variation of refractive index, it is called graded index medium. The early investigations in participating media are restricted to constant refractive index. However, in many engineering and practical problems, the medium has a variable refractive index such as heating of glass, thermal protecting coating, manufacturing of waveguide materials, ray transporting through atmosphere, optical measurement of flame [5], thermal barrier coating, connectors, electrochoromic displays, sensors, bobbins circuit breaker, batteries, electrochoromic windows, etc. [6]. The variation of refractive index may be as a result of the structure or thermal effect caused by spatial and temporal variations.

Refractive index and its variations depend on structure, chemical composition, thermal treatment and conditions, etc. Mass density, molecular polarizability and molecular weight are some parameters that affect the refractive index. For pure materials, the relation between these four quantities has been presented by Lorenz-Lorenz relation. [7]. Among these parameters, the effect of mass density on refractive index is dominant. For mass density <<1 the refractive index varies linearly with mass density [7]. The manufacturing process also affects refractive index. Photo-thermo-refractive (PTR) glass is an optical material that is a candidate for hologram writing. After UV-exposure and thermal treatment, local refractive changes are seen in PTR glass. This change can be a reason of local chemical changes and local residual stresses [8]. A study was down by Lumeau et al [8] shows that among these parameters, residual stresses are the main reason of local decrease of refractive index. [8]. Chemical composition can be another reason of the variation of refractive index. Aeropolymer are porous materials with low refractive index of 1.2-1.3. Polymide has high refractive index of 1.66. These materials do not have adjustable refractive index over wide range. Xerogels is a poor material that its refractive index can be adjusted by controlling the pore fraction or embedded micro or nano particles. Lisinki et al. [9,10] showed that mixed silica-titania xerogels and pure titania xerogels have tunable refractive index over wide range of 1.2-2.1.

Inverse analyses in radiative transfer are very important and have a lot of practical applications, such as remote sensing of atmosphere properties, the prediction of the temperature profile in a furnace or atmosphere or flame. As already mentioned, the radiative heat transfer in a semitransparent graded index medium has a lot of practical applications. Therefore, the inverse analysys of such media are also practical and important. First, we discussed about the direct problem of radiative transfer in graded index medium, since solving direct problem is a part of all inverse algorithms. Then we discuss the inverse problem.

1.4.1. Direct Problem of Radiative Transfer in Graded Index Medium

The first idea of solving radiative transfer equation (RTE) in graded index medium was to divide the medium to layers and in each layer the refractive index has a constant value. Such method can be found in the works of Siegle and Spuckler [11, 12] By the same idea of dividing the layer with variable refractive index to sub layers with constant refractive index, Xia et al. [13] analyzed the thermal emission and volumetric absorption in a graded index semitransparent medium. More complicated situation of steady and transient coupled radiativeconductive heat transfer in a graded index slab was studied by Yi et al. [14].

Curved ray tracing technique that was developed by Ben Abdolah and Dez [15-19] is another method of modeling radiative transfer in graded index medium. This technique was modified and extended by other investigators. Huange et al. [20] using a pseudo-source adding method combined with curved ray tracing technique and obtained the temperature field inside an absorbing-emitting graded index semi-transparent slab with diffuse gray walls in the radiative equilibrium. In this work the variation of refractive index was assumed to be linear. This combination was to deduce the radiative intensities on the gray walls. They also extended their method to account the arbitrary variation of refractive index by discretization of medium and assumption of local linear approximation for refractive index distribution. Two kinds of sinusoidal variation of refractive index were considered as the case studies [5]. Xia et al. [21] obtained the nondimensional radiative flux and temperature distribution in a semitransparent absorbing, emitting graded index slab. The modes of heat transfer were radiation